

Chapter 4

Examples

Identification of a reduced order controller for an active suspension

The discrete time identified model of the active suspension at the sampling frequency of $f_s = 800$ Hz is contained in the file `mods.mat`. The orders of the model are $n_A=6$, $n_B=8$ $d=0$ (the delay is contained in B) :

A =

```
1.0000 -1.6184 1.6617 -1.8469 1.6278 -1.3491 0.7239
```

B =

```
0 0 0 0 -0.3149 2.8144 -2.5972 -1.9891 2.0869
```

The model feature a double derivator behaviour and has three vibration modes.

The nominal robust controller (file `reg0.mat`) contains a fixed part $H_R = 1 + q^{-1}$. Its complexity is $n_R=11$ and $n_S=13$. For a standard pole placement, by solving the Bezout equation (with H_R), the resulting controller will have the orders : $n_R=5$, $n_S=7$ (but not robustness can be directly assured).

R =

Columns 1 through 7

```
0.0803 0.2609 0.4962 0.7528 0.9763 1.0760 1.0087
```

Columns 8 through 12

0.8360 0.5846 0.3350 0.1701 0.0555
S =

Columns 1 through 7

1.0000 2.1288 2.4944 2.8160 2.8554 2.0158 0.9458

Columns 8 through 14

-0.0408 -1.0447 -1.5059 -1.3851 -1.1084 -0.6337 -0.1600

To reduce the complexity of the controller we will use simulated data generated by the feedback connection of the plant model and the nominal controller. The external input is a PRBS generated by a 10-bit shift register with a clock frequency of $f_s/4$. (file excs.mat)

One uses the function :

» **[Rt,St,Table]=cor(r,B,A,R,S,[1 1],1,0.00125)**

This function itself uses conid with the default values. The results are summarized in the following table. The No. 0 corresponds to the nominal controller and the other numbers in the first column correspond to the various reduced order controller obtained for various n_R and n_S . All the controllers up to no. 7 can be used. The Vgap with respect to the nominal controller characteristics and nominal sensitivity functions remain small. No. 5 and no.7 have been selected. No;5 still verifies the Vinnicombe stability criterion (sufficient condition) and No.7 has the complexity of the pole placement design.

No.	nR	nS	Vg(R/S)	Vg(Sup)	Vg(Syp)	St-margin	Max(Syp)[fmax]	stable
0	11	13	0.0000	0.0000	0.0000	0.0756	5.55[81.90]	1
1	11	13	0.0352	0.0336	0.0707	0.0763	5.56[81.90]	1
2	10	12	0.0362	0.0334	0.0678	0.0826	5.56[81.90]	1
3	9	11	0.0365	0.0586	0.1578	0.0645	5.56[81.90]	1
4	8	10	0.0441	0.0451	0.0838	0.0849	5.56[81.90]	1
5	7	9	0.0390	0.0414	0.1221	0.0692	5.55[81.90]	1
6	6	8	0.3349	0.0708	0.2239	0.0552	5.62[81.90]	1
7	5	7	0.1873	0.1353	0.1191	0.0719	5.55[81.90]	1
8	4	6	1.0000	1.0000	1.0000	0.0000	20.74[167.46]	0
9	3	5	0.9566	1.0000	0.9843	0.0000	6.38[170.97]	0
10	2	4	0.4587	1.0000	1.0000	0.0000	6.51[86.26]	0
11	1	3	0.4240	0.3787	0.3685	0.0550	9.60[77.77]	1
12	1	2	0.4132	0.3421	0.5279	0.0307	11.79[176.37]	1
13	1	1	0.4446	0.1961	0.3991	0.0491	8.71[181.94]	1
14	1	0	0.5359	0.5124	0.5915	0.0836	6.30[201.81]	1

The characteristics of the various controllers can be compared by using compcon function.

compcon(B,A,Rt,St,[0,5,7])

The following figures show a comparison of the frequency characteristics of the various controllers (0,5,7) and the achieved output sensitivity and input sensitivity functions. One can observe that the characteristics of the reduced order controllers is very close to those of the nominal controller, particularly in the low frequencies up to 0.25 fs. Note that the PRBS used enhances the frequencies below 0.25fs.





